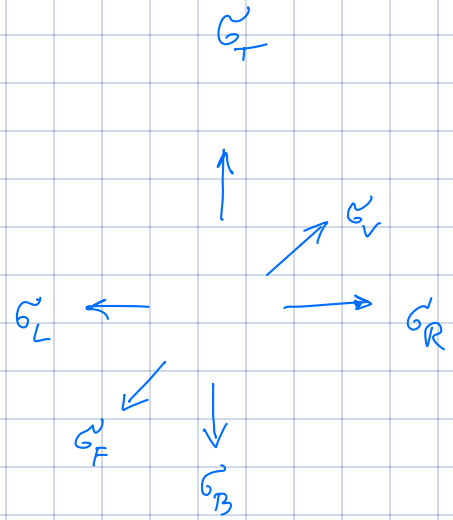
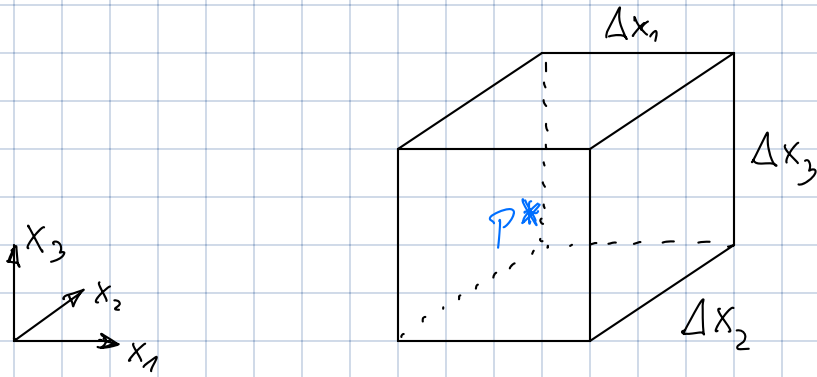


Regarding modelling

$$\text{Box} \subset \Omega \subset \mathbb{R}^3$$



$$P(x_1, x_2, x_3)$$

$$\vec{n} = \begin{pmatrix} n_1 \\ n_2 \\ n_3 \end{pmatrix}, \quad \nabla = \begin{pmatrix} \frac{\partial}{\partial x_1} \\ \frac{\partial}{\partial x_2} \\ \frac{\partial}{\partial x_3} \end{pmatrix}, \quad \frac{\partial u}{\partial \vec{n}} = \vec{n}^T \nabla u = \sum_{i=1}^d \frac{\partial}{\partial x_i} n_i$$

$\|\vec{n}\| = 1$, outward

Fourier law for orthotropic material

$$G_i = -\lambda_i \frac{\partial u}{\partial x_i}$$

or in general

$$\vec{G} = -\underline{\Lambda} \nabla u \quad (*)$$

[on boundary: $G_n = \vec{n}^T \vec{G}$, orthogonal to edge/surface]

diff. formulation energy balance

$$\rightarrow -\overset{\text{div}}{\nabla^T} \underline{\Lambda} \overset{\text{grad}}{\nabla} u = f(x) \text{ in } \Omega \quad + \text{B.C.} \quad (**)$$

$$\underline{\Lambda} = \underline{Id} \Rightarrow \nabla^T \nabla = \Delta = \sum_{i=1}^n \frac{\partial^2}{\partial x_i^2}$$

Laplace operator

Integral formulation Energy balance

(***)

$$-\int_{\partial\Omega_B} \sigma_B \cdot \vec{n} - \int_{\partial\Omega_T} \sigma_T \cdot \vec{n} - \int_{\partial\Omega_L} \sigma_L \cdot \vec{n} - \int_{\partial\Omega_R} \sigma_R \cdot \vec{n} - \int_{\partial\Omega_F} \sigma_F \cdot \vec{n} - \int_{\partial\Omega_V} \sigma_V \cdot \vec{n} + \underbrace{\int_{\Omega} f(\vec{x}) dx}_{\text{internal energy production}} = 0$$

energy outflow

internal energy production

(*)

$$\int_{\partial\Omega} (\underbrace{\Lambda \nabla u}_{\vec{F}}) \cdot \vec{n} ds$$

$$- \int_{\Omega} \nabla^T \underbrace{\Lambda \nabla u}_{\vec{F}} dx = 0$$

↓

$$\boxed{\int_{\partial\Omega} \vec{F} \cdot \vec{n} ds = \int_{\Omega} \underbrace{\nabla^T \vec{F}}_{\text{div}} dx}$$

Theorem by

Gauß -

Ostrogradski

|||

energy balance

(***) is the basis for Finite Volume Methods (FDM)

1st stationary heat conductivity problem

$$c(x) \rho(x) \frac{\partial u(x,t)}{\partial t} - \nabla^T \underbrace{\Lambda}_{\substack{\text{specific heat conductivity} \\ (x,t) \in \Omega \times T = Q_T \\ \text{space time cylinder}}} \nabla u(x,t) = f(x,t)$$

$c(x)$ specific heat capacity
 $\rho(x)$ density

+ b.c. , e.g. $u(x,t) = g_1(x,t)$

+ initial condition $u(x,0) = u_0(x)$

! Compatibility between b.c. and i.c. ✓

• $u(x,t) \in C^{2,1}(Q_T) \cap C^{1,0}((\Omega \cup \Gamma_2 \cup \Gamma_3) \times (0,T)) \cap C(\bar{Q}_T)$

• additional Terms:

- advection

$$+ q(x,t) \cdot u(x,t)$$

- convection

$$+ \vec{v}(x,t) \nabla u(x,t)$$

- radiation in b.c.

$$-(\Lambda \nabla u) \cdot n = \mu (u - u_{\text{ext}})^4$$