

Coffee Mug. We consider the time dependent heat conductivity problem

$$\begin{aligned} c(x) \frac{\partial u(x, t)}{\partial t} - \nabla_x^T (\lambda(x) \nabla_x u(x, t)) &= f(x, t) \quad (x, t) \in \Omega \times (0, T] \\ -\lambda(x) \frac{\partial u(x, t)}{\partial \vec{n}} &= \alpha(x) (u(x, t) - u_{out}(x, t)) \quad (x, t) \in \partial\Omega \times (0, T] \\ u(x, 0) &= u_0(x) \quad x \in \bar{\Omega} = \bar{\Omega}^{wall} \cup \bar{\Omega}^{fluid} \cup \bar{\Omega}^{air} \end{aligned} \quad (1)$$

with the initial condition $u_0(x, 0)$ and $x = (x_1, x_2, x_3)$.

The domain of interest Ω is my coffee mug with the geometry:



geometry	quantity	math	physics
lower (outer) diameter	50 mm	c	heat storage capacity
upper (outer) diameter	83 mm	λ	thermal conductivity
height	105 mm	f	internal heat sources
wall thickness	3 mm	α	heat transfer coefficient
bottom thickness	6 mm	u_{out}	outside temperature
height of coffee/water-fluid	66 mm	u_0	initial temperature

Figure 1: Domain of interest. It consist of 3 different regions: The ceramic mug Ω^{wall} itself, the inner part with fluid Ω^{fluid} and the air region between surface of fluid and the top edge of the cup Ω^{air} . The appropriate material coefficients c , λ , α differ with respect to the various subdomains. There are no inner heat sources f and only Robin boundary conditions¹ are assume.

We assume that all coefficients above do not change in time or depend on the solution u and we do not consider heat radiation. Otherwise we will end up with a non-linear problem. That excludes also density driven convection in Ω^{air} .

Simulations. The following general effects should be investigated to certain extend.

- (i) The initial temperature of the cup is the same as the surrounding air $u_0^{air,wall} = 18^\circ\text{C}$. The cup is filled with warm water such that $u_0^{fluid} = 80^\circ\text{C}$.
Q: How long does it take (T_{warm}) until the mug is heated to the optimal temperature² of 67°C ? What changes with $u_0^{fluid} = 80^\circ\text{C}$?
- (ii) We replace the water in the mug by coffee with temperature 85°C at time T_{warm} .
Q: How long does it take until the temperature of the coffee drops to 50°C ?
- (iii) You try to cool the coffee via blowing with velocity³ $2 \frac{m}{s}$ at the top edge. The temperature of your breath is 31°C .
Q: How much faster does the coffee cool down?

Presentation of results. In your git-repository, similar to evacuation of bees⁴.

¹https://en.wikipedia.org/wiki/Robin_boundary_condition

²<https://www.beanarella.at/de/welt-des-kaffees/kaffeetipps/die-perfekte-kaffeetemperatur>

³<https://www.atemmuskelttraining.com/de/patienten/normokapnische-hyperpnoe/>

koerperliche-leistung-atmung

⁴https://github.com/Mohadese561/Evacuation_of_Bees

Project A: Rotationally symmetric conductivity

Let us consider the mug without the handle so that we achieve the rotationally symmetric geometry Ω^{rot} .

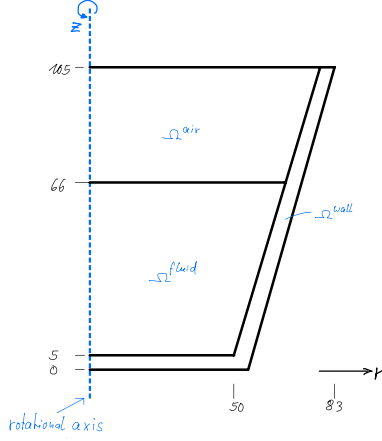


Figure 2: Ω^{rot} : rotationally symmetric

The transformation of coordinates $((x_1, x_2, x_3) \rightarrow (\varphi, r, z))$ and the assumption that no quantity is a function of φ results in the **rotationally symmetric** PDE

$$\begin{aligned}
 rc(\cdot) \frac{\partial u(\cdot, t)}{\partial t} - \nabla_{(r,z)}^T (r \lambda(\cdot) \nabla_{(r,z)} u(\cdot, t)) &= r f(\cdot, t) \quad (\cdot, t) \in \Omega^{rot} \times (0, T] \\
 -r \lambda(\cdot) \frac{\partial u(\cdot, t)}{\partial \vec{n}} &= r \alpha(\cdot) (u(\cdot, t) - u_{out}(\cdot, t)) \quad (\cdot, t) \in \Gamma^{robin} \times (0, T] \\
 \lambda(\cdot) \frac{\partial u(\cdot, t)}{\partial \vec{n}} &= 0 \quad (0, z, t) \in \Gamma^{symm} \times (0, T] \\
 u(\cdot, 0) &= u_0(\cdot) \quad (\cdot) \in \bar{\Omega} = \bar{\Omega}^{wall} \cup \bar{\Omega}^{fluid} \cup \bar{\Omega}^{air}
 \end{aligned} \tag{2}$$

with the initial condition $u_0(\cdot, 0)$, the symmetry boundary $\Gamma^{symm} := \{(r, z) : r = 0\}$, the Robin boundary $\Gamma^{robin} := \partial\Omega^{rot} \setminus \Gamma^{symm}$.

1. Generate the 2D mesh with the 3 material domains Ω^{wall} , Ω^{fluid} , Ω^{air} .
Derive the geometry description by changing [generate_mesh/chip_2materials.m](#) and using [shm/generate_mesh.m](#) matlab.
The script above generates two files *chip_2materials.txt* (coordinates of vertices and the finite element connectivity) and *chip_2materials_sd.txt* (material number per element).
2. Follow the code structure in [mgrid_2/main.cpp](#) for the Jacobi branch (`#undef MG`) and check whether the stationary Dirichlet problem can be solved. [shm/mgrid_2](#)
3. Implement for class `FEM_Matrix` a new Method `CalculateLaplace_mult` derived from `CalculateLaplace` that takes into account constant but different conductivities for your domains.

4. Change the boundary conditions from Dirichlet b.c. to Robin b.c..
Derive a method `ApplyRobinBC_mult` from `ApplyDirichletBC` in class `FEM_Matrix`.
5. Implement for class `FEM_Matrix` a new Method `CalculateLaplace_mult_rot` and a method `ApplyRobinBC_mult_rot` that realize the finite element matrix computation for the Laplace part (without $\frac{\partial u}{\partial t}$) in equ. (2).
6. Implement a method `AddMass_mult_rot` that realizes internally the calculation of the mass matrix entries $M_{i,j} := \int \int \textcolor{blue}{r} c(r, z) \phi_i \phi_j dr dz$ similar to the element calculation for the Laplace part of the matrix $K_{i,j}$ and adds it to the existing matrix entries.
7. Write a function (or method) `Init_Solution_mult` that initializes the solution in the whole domain depending on the subdomain. That function might be useful in subtask (i) as well as in (ii).
8. Use an explicit scheme to discretize in time so that we end up with the discrete formulation of (2)

$$\left(\frac{1}{\tau}M + K\right) \underline{u}^{k+1} = \underline{f}^{k+1} + \frac{1}{\tau}M \cdot \underline{u}^k \quad (3)$$

with τ denoting the chosen time step.

9. Solve (3) for subtask (i).

We consider a 2D cut of the mug as in Fig. 2 without rotation and without symmetry axis. The PDE is similar to (1) in x - and z -coordinates in Ω^{2d} .

1. Generate the 2D mesh with the 3 material domains Ω^{wall} , Ω^{fluid} , Ω^{air} .
Derive the geometry description by changing *generate_mesh/chip_2materials.m* and using matlab.
2. Follow the code structure in *mgrid_2/main.cpp* for the Jacobi branch (`#undef MG`) and check whether the stationary Dirichlet problem can be solved.
3. Implement for class `FEM_Matrix` a new Method `CalculateLaplace_mult` derived from `CalculateLaplace` that takes into account constant but different conductivities for your domains.
4. Change the boundary conditions from Dirichlet b.c. to Robin b.c..
Derive a method `ApplyRobinBC_mult` from `ApplyDirichletBC` in class `FEM_Matrix`.
5. Implement a method `AddMass_mult` that realizes internally the calculation of the mass matrix entries $M_{i,j} := \int \int c(x,z) \phi_i \phi_j dx dz$ similar to the element calculation for the Laplace part of the matrix $K_{i,j}$ and adds it to the existing matrix entries.
6. **Couple** the top edge of the mug from Ω^{2d} with a CFD problem (air stream) in a rectangular domain Ω^{CFD} . Modelling air as fluid is not fully correct but good enough for our purpose of coupling two PDE solvers.
 - Use the given solver for the heat conductivity problem shm/mgrid_2
 - Use OpenFoam for the CFD part (intro⁵, tutorial⁶, download⁷)
 - Use preCICE for coupling (intro⁸, docu⁹, quickstart¹⁰, adapters¹¹, fluid-temperature¹²).
Have a look at the example code in `f90`, especially files *precice_config.xml* and *main_precice.f90* . shm/mch

Start with one time step for the stationary problem.

7. Solve the coupled time-dependent problem.

⁵<https://www.openfoam.com/>

⁶<https://www.openfoam.com/documentation/tutorial-guide>

⁷<https://www.openfoam.com/current-release>

⁸<https://precice.org/>

⁹<https://precice.org/docs>

¹⁰<https://precice.org/quickstart>

¹¹<https://precice.org/adapters-overview>

¹²<https://precice.org/tutorials-flow-over-heated-plate>

Discretize and solve the full 3D problem using [ngsolve](https://ngsolve.org/)¹³. Consider the mug without handle as domain Ω .

ngsolve

1. Login to the jupyter hub¹⁴ on mephisto and start the ngsolve kernel.
2. Have a look at the tutorials¹⁵ and try some of them in the jupyter hub.
3. Find out how to describe the geometry¹⁶ and how produce a 3d mesh from it.
Start with the 2D geometry from Task A or B for the first experiments.
4. Solve the stationary heat conductivity problem (Laplace-like from (1)) in Ω .
5. Solve the instationary heat conductivity problem (1).
6. Try the coupling with CFD in the top surface of the mug.

netgen

¹³<https://ngsolve.org/>

¹⁴<https://imsc.uni-graz.at/jupyter>

¹⁵<https://docu.ngsolve.org/latest/i-tutorials/index.html>

¹⁶<https://docu.ngsolve.org/latest/i-tutorials/unit-4.1.1-geom2d/geom2d.html>

Riser-Cast-Sand. We consider a domain $\bar{\Omega} = \bar{\Omega}^{RS} \cup \bar{\Omega}^C \cup \bar{\Omega}^S$ with 3 sorts of physical effects, see Fig. 3-left. The FORTRAN-code by Diego Vasco¹⁷ is able to handle rectangular domains (Sleeve-Riser Ω^{RS} , Cube with all physics Ω^C) as depicted in Fig. 3-right. Although a simple

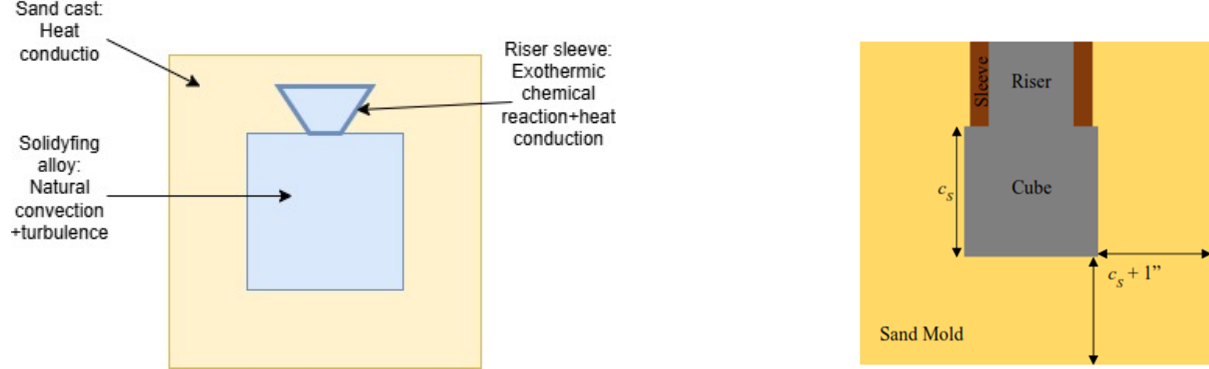


Figure 3: left: original domain; right: simplified domain

heat conductivity equation, the sand domain Ω^S cannot be handled by Vasco's solvers and so a second solver for the heat conductivity is needed. Therefore, we have to consider a coupling of the two codes via software *preCICE*.

- We assume Robin b.c. for the outer boundary of Γ^S .

$$-\lambda(x) \frac{\partial u(x, t)}{\partial \vec{n}} = \alpha(x) (u(x, t) - u_{out}(x, t)) \quad (x, t) \in (\partial\Omega^S \cap \partial\Omega) \times (0, Z]$$

- $\lambda = 0.27 \frac{W}{mK}$ (or assume 80%-dry Sandy Soils¹⁸ from saturated soils?)
- $\alpha = 10 \frac{W}{m^2K}$
- $u_{out} = 290K$
- no internal source, i.e. $f = 0$.

¹⁷<https://sciprofiles.com/profile/842146>

¹⁸https://en.wikipedia.org/wiki/List_of_thermal_conductivities

We are going to solve the problem on page 6 using code *CUBE_3D_Turbulent* and combine it with *OpenFoam* in 3D.

2026_Vasco/CUBE

1. Run the code *CUBE_3D_Turbulent*.
2. Determine the geometry of Ω^S .
3. Set up *OpenFoam* for the heat conductivity part in Ω^S with Dirichlet b.c. on Γ^S . (intro¹⁹, tutorial²⁰, equations²¹ download²²)
4. **Couple** the two solvers via *preCICE*.
 - Use the given solver for the heat conductivity problem
 - Use *preCICE* for coupling (intro²³, docu²⁴, quickstart²⁵, adapters²⁶, fluid-temperature²⁷).
 - Have a look at the example code in f90, especially files *precice-config.xml* and *main-precice.f90*.

shm/mgrid_2

shm/mch

Start with one time step for the stationary problem.

5. Solve the coupled time-dependent problem.

¹⁹<https://www.openfoam.com/>

²⁰<https://www.openfoam.com/documentation/tutorial-guide>

²¹<https://doc.openfoam.com/2312/tools/processing/numerics/schemes/>

²²<https://www.openfoam.com/current-release>

²³<https://precice.org/>

²⁴<https://precice.org/docs>

²⁵<https://precice.org/quickstart>

²⁶<https://precice.org/adapters-overview>

²⁷<https://precice.org/tutorials-flow-over-heated-plate>

We are going to solve the problem on page 6 using code *CUBE_RISER_SLEEVE_2D* and combine it with our adapted teaching code for the rotational symmetric heat equation (2) from page 2 in Ω^S .

2026_Vasco/CUBE

1. Run the code *CUBE_RISER_SLEEVE_2D*.
2. Determine the geometry of Ω^S .
3. Setup/Change the teaching solver:
 - (a) Generate the 2D mesh with the material domain Ω^S .
Derive the geometry description by changing [generate_mesh/chip_2materials.m](#) and using matlab.
The script above generates two files *chip_2materials.txt* (coordinates of vertices and the finite element connectivity) and *chip_2materials.sd.txt* (material number per element).
 - (b) Follow the code structure in [mgrid_2/main.cpp](#) for the Jacobi branch (`#undef MG`) and check whether the stationary Dirichlet problem can be solved.
 - (c) Change the boundary conditions from Dirichlet b.c. to Robin b.c..
Derive a method `ApplyRobinBC` from `ApplyDirichletBC` in class `FEM_Matrix`.
 - (d) Implement for class `FEM_Matrix` a new Method `CalculateLaplace_rot` and a method `ApplyRobinBC_rot` that realize the finite element matrix computation for the Laplace part (without $\frac{\partial u}{\partial t}$) in equ. (2).
 - (e) Implement a method `AddMass_rot` that realizes internally the calculation of the mass matrix entries $M_{i,j} := \int \int r c(r, z) \phi_i \phi_j dr dz$ similar to the element calculation for the Laplace part of the matrix $K_{i,j}$ and adds it to the existing matrix entries.
 - (f) Use an explicit scheme to discretize in time so that we end up with the discrete formulation of (2)

shm/generate_mesh

shm/mgrid_2

$$\left(\frac{1}{\tau}M + K\right) \underline{u}^{k+1} = \underline{f}^{k+1} + \frac{1}{\tau}M \cdot \underline{u}^k \quad (4)$$

with τ denoting the chosen time step.

- (g) Solve (3).
4. **Couple** the two solvers via *preCICE*.
 - Use the changed solver for the heat conductivity problem
 - Use preCICE for coupling (intro²⁸, docu²⁹, quickstart³⁰, adapters³¹, fluid-temperature³²).
 - Have a look at the example code in f90, especially files *precice_config.xml* and *main_precice.f90*.

shm/mgrid_2

shm/mch

Start with one time step for the stationary problem.

5. Solve the coupled time-dependent problem.

²⁸<https://precice.org/>

²⁹<https://precice.org/docs>

³⁰<https://precice.org/quickstart>

³¹<https://precice.org/adapters-overview>

³²<https://precice.org/tutorials-flow-over-heated-plate>