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MRI pulse design via discrete-valued optimal control

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Magnetic resonance imaging (MRI):

- popular for medical imaging (and spectroscopy)
- safe, radiation-free
- versatile
- simple image reconstruction (Fourier transform)
- but: complicated physics (compare CT: simple physics, complicated mathematics)

Basic steps in MR scan:

- 1 magnetic field is applied, aligns proton spins
- 2 radio pulse at resonance frequency is absorbed by hydrogen nuclei, re-radiated over time at same frequency
- 3 decaying time-dependent signal is measured by receiver coil

Fundamental principles of MRI:

- signal amplitude proportional to hydrogen density
- signal frequency proportional to magnetic field strength

Problem:

measured time-dependent signal is composite over whole volume, no spatial information

Solution:

use spatially dependent magnetic fields to map resonance frequency to spatial location

But: linear superposition of (x, y, z) fields is not unique

 \rightarrow sequential application of fields to encode (x, y, z) separately

Spatial encoding

Slice selection (z):

use z-proportional magnetic field during RF excitation

 $\blacksquare \rightsquigarrow$ only thin slice has resonance at RF pulse frequency, contributes to measured signal

Not considered here:

Frequency encoding (x):

use x-proportional magnetic field during measurement

Phase encoding (y):

 use y-proportional magnetic field before measurement to change phase offset of signal

 \rightsquigarrow FFT of time/phase-dependent data gives image

\rightsquigarrow MRI is controlled imaging \rightsquigarrow optimal control



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Mathematical model

Bloch equation

$$\frac{d}{dt}M(t) = \gamma M(t) \times B(t) + R(M(t)), \qquad M(0) = M_0$$

- $M(t) \in \mathbb{R}^3$ describes temporal evolution of spin ensemble
- **B**(t) controlled time-dependent magnetic field
- ightarrow γ gyromagnetic ratio ightarrow resonance frequency $ω = γB_0$

$$R(M) = \left(-M_x \frac{1}{T_2}, -M_y \frac{1}{T_2}, (-M_z - M_0) \frac{1}{T_1}\right)^T$$
 relaxation term
(T_1, T_2 tissue parameters)

Mathematical model

Slice selection (in rotating frame):

$$B(t) = (u_x(t)B_1, u_y(t)B_1, G_z(t)z)^T$$

 $G_z(t)$ slice-selective gradient field, B_1 static magnetic field

Bloch equation $\begin{cases}
\frac{d}{dt}M(t;z) = A(u(t);z)M(t;z) + b(z), & t > 0, \\
M(0;z) = M^{0}(z),
\end{cases}$

$$A(u;z) = \begin{pmatrix} -\frac{1}{T_2} & \gamma G_z(t)z & \gamma u_y(t)B_1 \\ -\gamma G_z(t)z & -\frac{1}{T_2} & \gamma u_x(t)B_1 \\ -\gamma u_y(t)B_1 & -\gamma u_x(t)B_1 & -\frac{1}{T_1} \end{pmatrix} \qquad b(z) = \begin{pmatrix} 0 \\ 0 \\ \frac{M_0}{T_1} \end{pmatrix}$$

Optimal control problem

Goal:

- compute control $u(t) = (u_x(t), u_y(t))$ such that $M(T) \approx M_d$
- \rightsquigarrow control-to-state mapping $S^{(\omega)}: u \to M(T; z)$
- $M_d(z)$ desired magnetization state \rightarrow slice selection
- $(M_d = M_d^{(\omega)})$ selective to resonance frequency \rightarrow spectroscopy)
- in addition: control with minimal specific absorption rate (SAR)

$$\min_{u \in L^2} \frac{1}{2} \sum_{\omega} \int_{-\alpha}^{\alpha} \left| S^{(\omega)}(u) - M_d^{(\omega)} \right|_2^2 dt + \frac{\alpha}{2} \int_0^T |u(t)|_2^2 dt$$

Numerical solution: gradient method

Gradient method

$$u^{k+1} = u^k - s^k g(u^k)$$

gradient

$$g(u^{k})(t) = \alpha u(t) + \gamma B_{1} \left(\int_{-\alpha}^{\alpha} M_{z}(t;z) P_{y}(t;z) - M_{y}(t;z) P_{z}(t;z) dz \right) \\ \int_{-\alpha}^{\alpha} M_{z}(t;z) P_{x}(t;z) - M_{x}(t;z) P_{z}(t;z) dz \right)$$

adjoint state solving (backward in time)

$$\begin{cases} -\frac{d}{dt}P(t;z) = A(u(t);z)^{T}P(t;z), & 0 \le t < T, \\ P(T;z) = M(T;z) - M_{d}(z), \end{cases}$$

step length s^k (Armijo, backtracking)

Numerical solution: Newton method

Newton method

$$H(u^k)\delta u=-g(u^k),\qquad u^{k+1}=u^k+\delta u$$

$$[H(u^k)h](t) = \alpha h(t) + \begin{pmatrix} \int_{-\alpha}^{\alpha} \delta M(t;z) A_1 P(t;z) + M(t;z) A_1 \delta P(t;z) dz \\ \int_{-\alpha}^{\alpha} \delta M(t;z) A_2 P(t;z) + M(t;z) A_2 \delta P(t;z) dz \end{pmatrix}$$

 $MA_1P = \gamma B_1(M_zP_y - M_yP_z) \qquad MA_2P = \gamma B_1(M_zP_x - M_yP_y)$

linearized state

$$\begin{cases} \frac{d}{dt} \delta M(t;z) = A(u^{k};z) \delta M(t;z) + A'(h)M, & 0 < t \le T, \\ \delta M(0;z) = (0,0,0)^{T}, \end{cases}$$

Numerical solution: Newton method

Newton method

$$H(u^k)\delta u=-g(u^k),\qquad u^{k+1}=u^k+\delta u$$

$$[H(u^k)h](t) = \alpha h(t) + \begin{pmatrix} \int_{-\alpha}^{\alpha} \delta M(t;z) A_1 P(t;z) + M(t;z) A_1 \delta P(t;z) dz \\ \int_{-\alpha}^{\alpha} \delta M(t;z) A_2 P(t;z) + M(t;z) A_2 \delta P(t;z) dz \end{pmatrix}$$

 $MA_1P = \gamma B_1(M_zP_y - M_yP_z) \qquad MA_2P = \gamma B_1(M_zP_x - M_yP_y)$

linearized adjoint

$$\begin{cases} -\frac{d}{dt}\delta P(t;z) = A(u^k;z)^T \delta P(t;z) + A'(h)^T P, & 0 \le t < T, \\ \delta P(T;z) = \delta M(T;z). \end{cases}$$

Numerical solution: Newton method

Bilinear control problem: non-convex

- solution of Newton step via CG method
- globalization by trust-region method (truncated CG [Steihaug])

Discretization:

- collocation points z_i (independent, parallel)
- Crank–Nicolson (state piecewise linear, controls piecewise constant)
- adjoint-consistent: adjoint state piecewise constant
- same for linearized state, adjoint
- CG method in weighted inner product (time steps)



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MR pulse design

Goal: multi-slice excitation

- initial magnetization $M_0 = (0, 0, 1)^T$
- gradient G_z from standard Cartesian sequence (2.56 ms)
- window a = 0.5 m, $\Delta z = 0.2 \text{ mm}$ (5001 points)

desired magnetization (slice width 5 mm)

$$M_d(z) = \begin{cases} (\sin(90^\circ), \cos(90^\circ), 0)^T & \text{in slice} \\ (0, 0, 1)^T & \text{out of slice} \end{cases}$$

• $u_0 \equiv (0,0)^T$, $\alpha = 10^{-4}$

Validation:

- implemented on 3T Siemens MR scanner
- phantom (slice profile homogeneity)
- healthy volunteer (image reconstruction)

Results: slice profile



Results: slice profile



Results: slice profile



Results: multi-slice excitation



Results: multi-slice excitation



Results: multi-slice excitation



Results: multi-slice reconstruction



Results: multi-slice reconstruction





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Technical limitation: device can only realize control from discrete set

$$U = \{ u \in L^2(0,T; \mathbb{R}^2) : u(t) \in \{u_1, \dots, u_d\} \text{ a.e.} \}$$

■ $u_1, \ldots, u_d \in \mathbb{R}^2$ given (fixed amplitude, phases)

non-convex discrete-valued control problem

$$\min_{u \in U} \frac{1}{2} \sum_{\omega} \|S^{(\omega)}(u) - M_d^{(\omega)}\|_2^2 + \frac{\alpha}{2} \int_0^T |u(t)|_2^2 dt$$

convex relaxation: replace U by convex hull

• works only for d = 2, cf. bang-bang control ($\alpha = 0$)

■ ~> promote $u(x) \in \{u_1, ..., u_d\}$ by convex pointwise penalty

$$\mathcal{G}(u) = \int_{\Omega} g(u(x)) \, dx$$

generalize L^1 norm: polyhedral epigraph with vertices u_1, \ldots, u_d

not exact relaxation/penalization (in general)!

generalize L^1 norm: polyhedral epigraph with vertices u_1, \ldots, u_d



- motivation: convex envelope of $\frac{1}{2} ||u||^2 + \delta_U$
- multi-bang (generalized bang-bang) control
- here: vector-valued control

Vector-valued multi-bang: penalty

Here: admissible control set U of d radially distributed states, origin

$$U = \left\{ \begin{pmatrix} 0 \\ 0 \end{pmatrix}, \begin{pmatrix} \omega_0 \cos \theta_1 \\ \omega_0 \sin \theta_1 \end{pmatrix}, \dots, \begin{pmatrix} \omega_0 \cos \theta_d \\ \omega_0 \sin \theta_d \end{pmatrix} \right\}$$

fixed amplitude
$$\omega_0 > 0$$

phases $0 \le \theta_1 < \ldots < \theta_d < 2\pi$
multi-bang penalty $g = \left(\frac{1}{2}|\cdot|_2^2 + \delta_U\right)^{**}$ convex envelope
 $g^*(q) = \left(\left(\frac{1}{2}|\cdot|_2^2 + \delta_U\right)^{**}\right)^* (q) = \left(\frac{1}{2}|\cdot|_2^2 + \delta_U\right)^* (q)$
 $= \begin{cases} 0 & \langle q, u_i \rangle \le \frac{1}{2}\omega_0^2 \text{ for all } 1 \le i \le d \\ \langle q, u_i \rangle - \frac{1}{2}\omega_0^2 & \frac{\theta_{i-1}+\theta_i}{2} \le \angle q \le \frac{\theta_i+\theta_{i+1}}{2}, \langle q, u_i \rangle \ge \frac{1}{2} \end{cases}$

Vector-valued multi-bang: subdifferential

Fenchel conjugate

$$g^*(q) = \begin{cases} 0 := u_0 & q \in \overline{Q}_0 \\ \langle q, u_i \rangle - \frac{1}{2}\omega_0^2 & q \in \overline{Q}_i \end{cases}$$

Subdifferential

$$\partial g^{*}(q) = \begin{cases} \{u_{i}\} & q \in Q_{i} & 0 \le i \le d \\ \cos\{u_{i_{1}}, \dots, u_{i_{k}}\} & q \in Q_{i_{1}\dots i_{k}} & 0 \le i_{1}, \dots, i_{k} \le d \end{cases}$$

Vector-valued multi-bang: subdifferential

Subdifferential

$$\partial g^*(q) = \begin{cases} \{u_i\} & q \in Q_i & 0 \le i \le d \\ \cos\{u_{i_1}, \dots, u_{i_k}\} & q \in Q_{i_1 \dots i_k} & 0 \le i_1, \dots, i_k \le d \end{cases}$$

Moreau-Yosida regularization

$$(\partial g^{*})_{\gamma}(q) = \begin{cases} u_{i} & q \in Q_{i}^{\gamma} \\ \left(\frac{\langle q, u_{i} \rangle}{\gamma \omega_{0}^{2}} - \frac{\alpha}{2\gamma}\right) u_{i} & q \in Q_{0,i}^{\gamma} \\ \frac{u_{i}+u_{i+1}}{2} + \frac{\langle q, u_{i}-u_{i+1} \rangle (u_{i}-u_{i+1})}{\gamma |u_{i}-u_{i+1}|_{2}^{2}} & q \in Q_{i,i+1}^{\gamma} \\ \frac{q}{\gamma} - \frac{\alpha}{\gamma} \left(\frac{\omega_{0}}{|u_{i}+u_{i+1}|_{2}}\right)^{2} (u_{i}+u_{i+1}) & q \in Q_{0,i,i+1}^{\gamma} \end{cases}$$

Vector-valued multi-bang: subdifferential





Vector-valued multi-bang: Newton method

Newton derivative

$$D_{N}(\partial g_{\gamma}^{*})(q) = \begin{cases} 0 & q \in Q_{i}^{\gamma} \\ \frac{u_{i}u_{i}^{T}1}{\gamma \omega_{0}^{2}} & q \in Q_{0,i}^{\gamma} \\ \frac{(u_{i}-u_{i+1})(u_{i}-u_{i+1})^{T}}{\gamma |u_{i}-u_{i+1}|_{2}^{2}} & q \in Q_{i,i+1}^{\gamma} \\ \frac{1}{\gamma} \operatorname{Id} & q \in Q_{0,i,i+1}^{\gamma} \end{cases}$$

Superposition operator:

$$\left[D_N H_{\gamma}(p)\right](t) \coloneqq D_N\left(\partial g_{\gamma}^*\right)(p(t)) \text{ a.e. } t \in [0,T]$$

Semismooth Newton system

$$\left(\operatorname{Id} - D_N H_{\gamma}(\mathcal{F}'(u^k))\mathcal{F}''(u^k)\right)\delta u = -u^k + \partial \mathcal{G}_{\gamma}^*(\mathcal{F}'(u^k))$$

matrix-free Krylov method for semismooth Newton step

- $\blacksquare \mathcal{F}', \mathcal{F}''$ via linearized, adjoint Bloch equation
- discretization, adjoint as before

goal: shift magnetization from $M_0 = (0, 0, 1)^T$ at t = 0to $M_d = (1, 0, 0)^T$ at t = T

d = 3, 6 radially distributed admissible control states

- n = 1, 4 isochromats with different resonance frequencies
 - shift all isochromats
 - 2 shift only one isochromat

$$\alpha = 10^{-1}, \omega_0 = 1$$

example motivated by [Dridi/Lapert/Salomon/Glaser/Sugny '15]



Figure: n = 1 isochromat, d = 3 control states



Figure: n = 1 isochromat, d = 6 control states



Figure: n = 4 isochromats, same target



Figure: J = 4 isochromats, different targets

Conclusion

Optimal control for MR pulse design

- allows designing low energy pulses
- allows incorporating full physical model
- allows accelerated imaging
- allows incorporating structural constraints

Outlook:

- joint optimization of RF pulse and gradient
- (joint) optimization of frequency, phase encoding
- joint optimization and reconstruction

Preprints, codes:

http://homepage.uni-graz.at/c.clason/publikationen